

KWIK HUS

REUSABILITY SYSTEM

The first and only reusable screw anchor in the market.



With the launch of the new Hilti Reusability Gauge (HRG), Hilti becomes the first manufacturer to allow and provide guidance for reusing its concrete screw anchors.

Screw anchor holding values are influenced by the ability of its threads to bear against the concrete. Reusing the anchor can reduce the diameter of the threads, thereby reducing the anchor's holding values. Hilti publishes load values for both single-use and reused anchors — and has developed matched-diameter "go/no-go" HRG gauges to verify the anchor is suitable for reuse.

With up to 20 reuses, the cost per fastening point can be significantly reduced, improving profitability and productivity.

This makes the KWIK HUS the first screw anchor that allows the installer to... **Drill. Drive. Done... Reuse**.

Productivity

- Removable and reusable, reducing the amount of anchors needed per project and cost per fastening point
- More than 50% installation time savings over coil and stud anchors
- Higher number of reuses allowed compared to coil anchors
- No additional coil component needed to purchase

Reliability

- Reusability gauge quickly identifies if the anchor is still within its useful life
- Published load capacity listings for reused anchors provide guidance to installers and engineers



Great for temporary bracing...

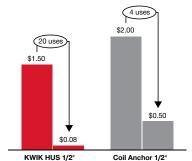


... and temporary railings





In the example below, using a 1/2" screw anchor after 20 uses drops the price per fastening point to just \$0.08. Coupled with the installation time savings of more than 50% when inserting a screw anchor versus a coil anchor, installing KWIK HUS screws with the HRG can lead to thousands of dollars in savings per project. Note: Number of reuses is dependent upon the anchor diameter and the concrete compressive strength.





Screw anchor KWIK HUS

Applications and advantages

- Attaching formwork and tilt-up braces, sill plates, perimeter walls
- Racking and shelving
- Attaching ledgers
- For use with standard ANSI-tolerance drill bit; no special tolerance drill bits are required
- Tested and evaluated according to AC 193 for uncracked concrete and AC 106 for grout-filled CMU blocks

Technical data	
Approvals / Test reports	Nuclear (NQA-1)
Environmental conditions	Indoor, dry conditions
Head configuration	Hex head
Installation direction	All
Material, corrosion	Steel, zinc-plated to a min. thickness of 8 µm
Type of fixing	Through-fastening



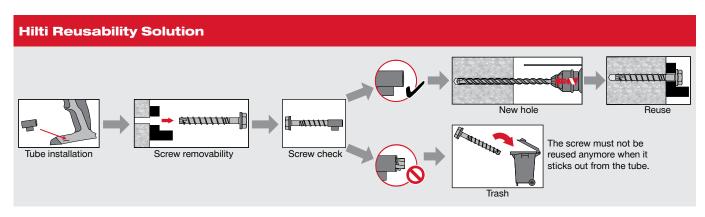
Screw anchor KWIK HUS order information

	Drill bit		Box	only	Master carton 1x		
Order Designation	diameter	Anchor length	Sales pack quantity	Item number	Sales pack quantity	Item number	
Screw anc KH 3/8" x 2-1/8"	3/8 in	2-1/8 in	50 pc	434436	450 pc	3465007	
Screw anc KH 3/8 x 3"	3/8 in	3 in	50 pc	434437	300 pc	3465008	
Screw anc KH 3/8" x 3-1/2"	3/8 in	3-1/2 in	50 pc	434438	300 pc	3465009	
Screw anc KH 3/8" x 4"	3/8 in	4 in	50 pc	434439	300 pc	3465010	
Screw anc KH 3/8" x 5"	3/8 in	5 in	30 pc	434440	270 pc	3465011	
Screw anc KH 1/2" x 3"	1/2 in	3 in	30 pc	434441	180 pc	3465012	
Screw anc KH 1/2" x 3-1/2"	1/2 in	3-1/2 in	25 pc	434442	150 pc	3465013	
Screw anc KH 1/2" x 4"	1/2 in	4 in	25 pc	434443	150 pc	3465014	
Screw anc KH 1/2" x 4-1/2"	1/2 in	4-1/2 in	25 pc	434444	150 pc	3465015	
Screw anc KH 1/2" x 5"	1/2 in	5 in	25 pc	434445	150 pc	3465016	
Screw anc KH 1/2" x 6"	1/2 in	6 in	25 pc	434446	150 pc	3465017	
Screw anc KH 5/8" x 4"	5/8 in	4 in	15 pc	434447	90 pc	3465018	
Screw anc KH 5/8" x 5-1/2"	5/8 in	5-1/2 in	15 pc	434448	90 pc	3465019	
Screw anc KH 5/8" x 6-1/2"	5/8 in	6-1/2 in	15 pc	434449	45 pc	3465020	
Screw anc KH 3/4" x 4-1/2"	3/4 in	4-1/2 in	10 pc	434450	60 pc	3465021	
Screw anc KH 3/4" x 5-1/2"	3/4 in	5-1/2 in	10 pc	434451	30 pc	3465022	
Screw anc KH 3/4" x 7"	3/4 in	7 in	10 pc	434452	40 pc	3465023	
Screw anc KH 3/4" x 9"	3/4 in	9 in	10 pc	434453	40 pc	3465024	

HRG - KWIK HUS anchor reusability gauge

Order Designation	Diameter	Sales pack quantity	Item number
Hilti reusability gauge HRG 3/8"	3/8 in	1 pc	2122554
Hilti reusability gauge HRG 1/2"	1/2 in	1 pc	2122555
Hilti reusability gauge HRG 5/8"	5/8 in	1 pc	2122556
Hilti reusability gauge HRG 3/4"	3/4 in	1 pc	2122557

The Hilti Reusability Gauge (HRG) indicates to the installer if the anchor has exceeded its useful life prior to installation.





Product Description

The Hilti Reusable Gauge (HRG) is a zinc-plated hollow steel tube used with the Hilti KWIK HUS screw anchor for reuse applications (e.g. concrete formwork, tilt-up bracing, temporary railings and opening coverings). Each KWIK HUS diameter has a corresponding HRG that is attached to Hilti impact wrenches. A KWIK HUS can be installed, used, and removed multiple times until the HRG indicates whether the threads in the anchor have been worn beyond its useful life. The concept is simple: if the KH does not pass through the length of the HRG, it can continue to be used with the "reused" published loads in this document being applicable.

Description of Technical Data

Testing and Product Evaluation

Hilti KWIK HUS screw anchors were continually reused in concrete until the screw threads met the lifetime limits as indicated by the HRG. The worndown KH screws were then tested in tension and shear and nominal capacities were determined based on ICC Evaluation Services (ICC-ES) Acceptance Criteria for Post-installed Mechanical Anchors in Concrete Elements (AC193), which incorporates the requirements of ACI 355.2-07.

Anchor Design Codes

- United States Design strength calculated using ACI 318-14 Chapter 17 or ACI 318-11 Appendix D.
- Canada Factored resistance calculated using CSA A23.3-14 Annex D.

Design of KWIK HUS Mechanical Anchor System with Hilti Reusable Gauge

Determination of Nominal Strengths (ACI) and Nominal Resistances (CSA)

The nominal strength (ACI), or nominal resistance (CSA), determined through testing according to AC193 / ACI 355.2 or calculation through ACI 318-11 Appendix D / CSA A23.3-14 Annex D is multiplied by strength modification factors, resulting in a design strength (ACI), or factored resistance (CSA), for the KH anchor. Design strengths (factored resistances) are provided in Table 3 of this document for KH anchors worn to the limits of the HRG inner diameters.

ACI:

- N_n = Nominal strength in tension (least of concrete, pullout, or steel strength)
- V_n = Nominal strength in shear (lesser of pryout or steel strength)
- φ = Strength reduction factor
- $\phi N_n =$ Design strength in tension
- ΦV = Design strength in shear

CSA:

- N_n = Nominal strength in tension (least of concrete, pullout, or steel strength)
- V_n = Nominal strength in shear (lesser of pryout or steel strength)
- φ = Material resistance factor
- R = Resistance modification factor
- $N_r = \text{Factored resistance in tension} = \phi N_a R$
- V_r = Factored resistance in shear = $\phi V_n R$

Because ACI and CSA limit the minimum concrete compressive strength to 2,500 psi (17.2 MPa) for calculation of the design strength (factored resistance), the published results for 2,000 psi (13.7 MPa) concrete are based on testing.



Interaction of Tension and Shear

Where anchors are loaded simultaneously in tension and shear, interaction must be considered. Applicable ACI 318-11 Appendix D and CSA A23.3-14 Annex D anchorage interaction equations are given below.

ACI:
$$\frac{N_{ua}}{\Phi N_n} + \frac{V_{ua}}{\Phi V_n} \le 1.2$$

Required strength in tension based on factored load combinations of ACI 318-11 Chapter 9

Required strength in shear based on factored load combinations of ACI 318-11 Chapter 9

CSA:
$$\frac{N_f}{N_r} + \frac{V_f}{V_r} \le 1.2$$

where:

= Required strength in tension based on factored load combinations of CSA A23.3-14 Chapter 8

= Required strength in shear based on factored load combinations of CSA A23.3-14 Chapter 8

The full tensile strength can be permitted if:

ACI:
$$\frac{V_{ua}}{\Phi V_{o}} \le 0.2$$
 CSA: $\frac{V_{f}}{V_{c}} \le 0.2$

The full shear strength can be permitted if:

ACI:
$$\frac{N_{ua}}{\Phi N_{a}} \le 0.2$$
 CSA: $\frac{N_{f}}{N_{r}} \le 0.2$

Allowable Stress Design

The design strength (factored resistance) values in Tables 2 and 3 can be converted to an Allowable Stress Design (ASD) value as follows:

$$N_{ASD} = \frac{\Phi N_n}{\propto_{ASD}}$$

$$V_{ASD} = \frac{\Phi V_n}{\approx_{ASD}}$$

where

∝_{ASD} = Conversion factor calculated as a weighted average of the LRFD load factors normalized by the ASD load factors for the controlling load combination. Guidance for calculation of \bowtie_{ASD} is given at:

http://www.icc-es.org/News/Notices/ES/SD-ASD_Letter.pdf.

Some examples of ∝_{ASD} for specific cases are provided

• Pure wind load: $\propto_{ASD,W} = 1.67$

• Pure live load: \approx_{ASDI} = 1.6

• Pure dead load: $\propto_{ASD,D}$ = 1.4

• 50% dead load, 50% live load: ∝_{ASD DI} = 1.4



Table 1 — Reused KWIK HUS installation parameters for temporary applications with the Hilti HRG1.

			Nominal anchor diameter (in.)											
Characteristic	Symbol	Units		3/8			1/2		5,	/8	3/4			
Nominal bit diameter	d _{bit}	in.		3/8			1/2		5,	/8	3/4			
Fixture hole diameter	٠,	in.		1/2			5/8		3,	/4	7/8			
Fixture note diameter	d _h	(mm)		(13)			(16)		(1	9)	(2	(22)		
Installation torque ²		ftlb.		40			45		8	35	1.	15		
installation torque	T _{inst}	(n-M)		(54)			(61)		(1	15)	(1	56)		
Impact wrench torque rating with $f'_c > 3,000 \text{ psi}^3$	_	ft lla	122	14	48	122	14	48	30	30	330			
Impact wrench torque rating with f'_c <3,000 psi ³	T _{impact}	ftlb. 44 100 100			148 330		330							
Nominal embedment	h	in.	1-5/8	2-1/2	3-1/4	2-1/4	3	4-1/4	3-1/4	5	4	6-1/4		
Nominal embedment	h _{nom}	(mm)	(41)	(64)	(83)	(57)	(76)	(108)	(83)	(127)	(102)	(159)		
Minimum hole depth	h _o	in.	1-7/8	2-3/4	3-1/2	2-5/8	3-3/8	4-5/8	3-5/8	5-3/8	4-3/8	6-5/8		
Will ill fluit floie deptil	",	(mm)	(41)	(70)	(89)	(67)	(86)	(117)	(92)	(137)	(111)	(168)		
Minimum edge distance in		in.	3-3/8	5-1/4	6	4-1/8	5-5/8	8-3/8	6-3/8	10	10	12-1/8		
direction of loading	C _{a1}	(mm)	(85)	(133)	(154)	(106)	(143)	(214)	(162)	(253)	(253)	(308)		
Minimum edge distance		in.	5	7-7/8	9-1/8	6-1/4	8-1/2	12-5/8	9-1/2	15	15	18-1/4		
parallel to load direction	C _{a2}	(mm)	(128)	(200)	(231)	(159)	(215)	(321)	(243)	(380)	(379)	(463)		
Minimum spacing		in.	4-7/8	7-1/2	9-3/4	6-3/4	9	12-3/4	9-3/4	15	12	18-3/4		
wiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiii	S _{min}	(mm)	(124)	(191)	(248)	(171)	(229)	(324)	(248)	(381)	(305)	(476)		
Minimum concrete thickness	h	in.	3-1/4	4	4-7/8	3-3/4	4-3/4	6-3/4	5	7	6	8-1/8		
Will ill fluit Concrete trickness	h _{min}	(mm)	(83)	(102)	(124)	(95)	(121)	(171)	(127)	(178)	(152)	(206)		
Wrench size	-	in.		9/16			3/4		15,	/16	1-	1-1/8		

¹ See Figure 1 for installation parameters intended for re-used KH measured with HRG.

 ^{2 7} inst applies to installations using a calibrated torque wrench.
 3 Torque ratings of Hilti impact tools. Because of variability in measurement procedures, the published torque of an impact tool may not correlate properly with the above setting torques. Over-torqueing can damage the anchor and/or reduce its holding capacity.

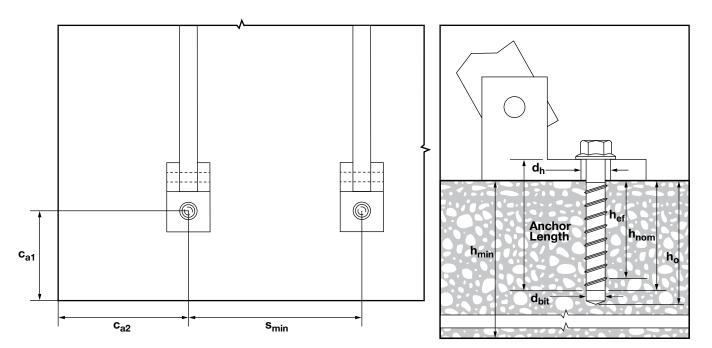


Figure 1 — Illustration of KWIK HUS installation parameters for reuse.



Table 2 — Single-use Hilti KWIK HUS design strength (factored resistance) in uncracked concrete^{1,2}. IMPORTANT: these values are higher as compared to a reused anchor.

Nominal		f' = 2000 psi (13.7 MPa)							f' _c = 4000 psi (27.5 MPa)							f' = 6000 psi (41.2 MPa)						
anchor diameter	nchor Nominal				Tension Shear ϕN_n or N_r ϕV_n or V_r		60-degree ⁵		Tension ϕN_n or N_r		Shear ϕV_n or V_r		60-degree⁵		Tension ϕN_n or N_r		Shear ϕV_n or V_r		60-de	egree ⁵		
in.	in.	(mm)	lb.	(kN)	lb.	(kN)	lb.	(kN)	lb.	(kN)	lb.	(kN)	lb.	(kN)	lb.	(kN)	lb.	(kN)	lb.	(kN)		
	1-5/8	(41)	815	(3.6)	880	(3.9)	735	(3.3)	1,155	(5.1)	1,245	(5.5)	1,040	(4.6)	1,415	(6.3)	1,520	(6.8)	1,275	(5.7)		
3/8	2-1/2	(64)	1,770	(7.9)	1,905	(8.5)	1,595	(7.1)	2,505	(11.1)	2,695	(12.0)	2,260	(10.1)	3,065	(13.6)	3,095	(13.8)	2,700	(12.0)		
	3-1/4	(83)	2,275	(10.1)	2,450	(10.9)	2,050	(9.1)	3,220	(14.3)	3,095	(13.8)	2,785	(12.4)	3,945	(17.6)	3,095	(13.8)	3,150	(14.0)		
	2-1/4	(57)	1,305	(5.8)	1,410	(6.3)	1,180	(5.2)	1,850	(8.2)	1,990	(8.9)	1,670	(7.4)	2,265	(10.1)	2,440	(10.9)	2,045	(9.1)		
1/2	3	(76)	2,215	(9.9)	2,385	(10.6)	2,000	(8.9)	3,130	(13.9)	3,375	(15.0)	2,825	(12.6)	3,835	(17.1)	4,130	(18.4)	3,460	(15.4)		
	4-1/4	(108)	3,375	(15.0)	4,910	(21.8)	3,350	(14.9	5,700	(25.4)	4,910	(21.8)	4,730	(21.0)	6,980	(31.1)	4,910	(21.8)	5,310	(23.6)		
F /0	3-1/4	(83)	2,900	(12.9)	3,120	(13.9)	2,615	(11.6)	4,100	(18.2)	4,415	(19.6)	3,700	(16.5)	5,025	(22.4)	5,410	(24.1)	4,530	(20.2)		
5/8	5	(127)	3,960	(17.6)	6,735	(30.0)	4,095	(18.2)	8,485	(37.8)	6,735	(30.0)	6,805	(30.3)	10,390	(46.2)	6,735	(30.0)	7,615	(33.9)		
2/4	4	(102)	3,340	(14.9)	8,435	(37.5)	3,765	(16.8)	5,540	(24.7)	9,995	(44.5)	5,815	(25.9)	6,785	(30.2)	9,995	(44.5)	6,755	(30.1)		
3/4	6-1/4	(159)	8,355	(37.2)	9,995	(44.5)	7,810	(34.8)	11,820	(52.6)	9,995	(44.5)	9,735	(43.3)	14,475	(64.4)	9,995	(44.5)	10,925	(48.6)		

¹ Tabulated values are based on the characteristic ultimate values obtained in testing for a Hilti KWIK HUS anchor installed for the first time in concrete. See the Description of Technical Data section for an explanation of how values were determined.

Table 3 — Reused Hilti KWIK HUS design strength (factored resistance) with the Hilti Reusability Gauge in uncracked concrete^{1,2}. IMPORTANT: these values are reduced as compared to a single-use anchor.

Nominal			f' = 2000 psi (13.7 MPa)							f' = 4000 psi (27.5 MPa)							f' = 6000 psi (41.2 MPa)					
anchor diameter	r Nominal		Tension ϕN_n or N_r		Shear ϕV_n or V_r		60-degree⁵		Tension ϕN_n or N_r		Shear ϕV_n or V_r		60-degree ⁵		Tension ϕN_n or N_r		Shear ϕV_n or V_r		60-de	gree⁵		
in.	in.	(mm)	lb.	(kN)	lb.	(kN)	lb.	(kN)	lb.	(kN)	lb.	(kN)	lb.	(kN)	lb.	(kN)	lb.	(kN)	lb.	(kN)		
	1-5/8	(41)	670	(3.0)	880	(3.9)	645	(2.9)	915	(4.1)	1,245	(5.5)	890	(4.0)	1,100	(4.9)	1,520	(6.8)	1,075	(4.8)		
3/8	2-1/2	(64)	970	(4.3)	1,905	(8.5)	1,040	(4.6)	1,370	(6.1)	2,695	(12.0)	1,470	(6.5)	2,395	(10.7)	3,095	(13.8)	2,295	(10.2)		
	3-1/4	(83)	2,160	(9.6)	2,450	(10.9)	1,985	(8.8)	2,705	(12.0)	3,095	(13.8)	2,490	(11.1)	2,870	(12.8)	3,095	(13.8)	2,590	(11.5)		
	2-1/4	(57)	955	(4.2)	1,410	(6.3)	950	(4.2)	1,350	(6.0)	1,990	(8.9)	1,345	(6.0)	1,955	(8.7)	2,440	(10.9)	1,850	(8.2)		
1/2	3	(76)	1,555	(6.9)	2,385	(10.6)	1,565	(7.0)	2,195	(9.8)	3,375	(15.0)	2,210	(9.8)	3,380	(15.0)	4,130	(18.4)	3,180	(14.2)		
	4-1/4	(108)	3,205	(14.3)	4,910	(21.8)	3,225	(14.4)	5,250	(23.4)	4,910	(21.8)	4,500	(20.0)	5,780	(25.7)	4,910	(21.8)	4,770	(21.2)		
E /0	3-1/4	(83)	2,225	(9.9)	3,120	(13.9)	2,185	(9.7)	3,145	(14.0)	4,415	(19.6)	3,090	(13.8)	4,280	(19.0)	5,410	(24.1)	4,070	(18.1)		
5/8	5	(127)	3,760	(16.7)	6,735	(30.0)	3,940	(17.5)	7,720	(34.4)	6,735	(30.0)	6,435	(28.6)	6,945	(30.9)	6,735	(30.0)	6,030	(26.8)		
2/4	4	(102)	2,195	(9.8)	6,695	(29.8)	2,555	(11.4)	3,100	(13.8)	6,695	(29.8)	3,390	(15.1)	6,445	(28.7)	6,695	(29.8)	5,740	(25.5)		
3/4	6-1/4	(159)	7,935	(35.3)	9,995	(44.5)	7,540	(33.6)	11,230	(50.0)	9,995	(44.5)	9,440	(42.0)	12,390	(55.1)	9,995	(44.5)	10,005	(44.5		

¹ Tabulated values are based on the characteristic ultimate values obtained in testing for a Hilti KWIK HUS anchor meeting the minimum diameter requirements as checked with the Hilti Reusability Gauge. See the Description of Technical Data section for an explanation of how values were determined.

² Tabulated values are for normal-weight concrete only. For lightweight concrete multiply design strength (factored resistance) by λ_a as follows: for sand-lightweight, λ_a = 0.68; for all-lightweight, λ_a = 0.60.

a Since ACI and CSA limit the concrete compressive strength to 2,500 psi (17.2 MPa) for calculation of the design strength (factored resistance), the published results for 2,000 psi (13.7 MPa) concrete are based on testing.

⁴ Design strength (factored resistance) in 4,000 psi (27.5 MPa) and 6,000 psi (41.2 MPa) concrete are based on test data and calculations according to ACI 318-11 Appendix D and CSA A23.3-14 Annex D.

^{5 60-}degree loads are calculated for a pinned connection where the load acts 60 degrees from a line parallel to the concrete surface using the interaction equation between tension and shear failure in the Description of Technical Data section with the tabulated tension and shear design strengths (factored resistances).

² Tabulated values are for normal-weight concrete only. For lightweight concrete multiply design strength (factored resistance) by λ_a as follows: for sand-lightweight, λ_a = 0.68; for all-lightweight, λ = 0.60.

lightweight, λ_s = 0.60.

3 Since ACI and CSA limit the concrete compressive strength to 2,500 psi (17.2 MPa) for calculation of the design strength (factored resistance), the published results for 2,000 psi (13.7 MPa) concrete are based on testing.

Design strength (factored resistance) in 4,000 psi (27.5 MPa) and 6,000 psi (41.2 MPa) concrete are based on test data and calculations according to ACI 318-11 Appendix D and CSA A23.3-14 Annex D.

^{5 60-}degree loads are calculated for a pinned connection where the load acts 60 degrees from a line parallel to the concrete surface using the interaction equation between tension and shear failure in the Description of Technical Data section with the tabulated tension and shear design strengths (factored resistances).



Hilti. Outperform. Outlast.

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The data contained in this literature was current as of the date of publication. Updates and changes may be made based on later testing. If verification is needed that the data is still current, please contact the Hilti Technical Support Specialists at 1-800-363-4458. All published load values contained in this literature represent the results of testing by Hilti or test organizations. Local base materials were used. Because of variations in materials, on-site testing is necessary to determine performance at any specific site. Laser beams represented by red lines in this publication. Printed in the United States

